Wire Bristle Impacting as an Alternative to Shot Peening for Improving Fatigue Performance

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Mechanical surface treatments such as shot peening, deep rolling and laser shock peening are well known to improve fatigue performance of metallic components. This improvement is often explained by the process-induced residual compressive stresses that reduce the propagation rate of surface cracks. Wire bristle impacting by rotating steel brushes is typically applied for descaling and deburring by which oxide layers are removed from heat treated steel components.

Up to now, wire bristle impacting is almost exclusively utilized for surface cleaning and preparation the surface for coating and/or painting. The effect of wire bristle impacting on possible surface strengthening and resulting fatigue strength enhancement was hardly taken into consideration.

In the present investigation, the effects of wire bristle impacting on the surface and surface layer properties such as surface roughness, work hardening and residual stress profiles are compared with shot peening effects on Al2024-T4. In addition, the high cycle fatigue performance of wire bristle impacted and shot peened conditions are compared and contrasted.

For shot peening, a universal peening machine Gravi 2000 of OSK Kiefer, Oppurg, was used (Fig. 1). Figure 2 illustrates the peening process on a fatigue specimen.





Figure. 1: Shot peening machine

Figure 2: Peening procedure

Spherically conditioned cut wire SCCW 14 was used.

Wire bristle impacting was utilized by an electrically driven system named Bristle Blaster[®] from Monti, Hennef (Fig. 3). The brushes were made of high strength spring steels.



Figure 3: Bristle Blaster® tool for wire bristle impacting

Before treating the fatigue specimens, the influence of the exposure time in wire bristle impacting as well as in shot peening on the curvature development of Almen strips was determined. Results are illustrated in Figure 4.





Both treatments led to marked increases in curvature of the used Almen strips type A already after short exposure times. As seen in Figure 4, the resulting curvatures after 300 s are about the same amounting to 0,15 mmA independent of the particular surface treatment. A comparison of the roughness values measured by a perthometer are given in Table 1

Wire bristle impacting	R _{max} (µm)	R _a (µm)	Shot peening	R _{max} (μm)	R _a (µm)
	34.0	3.8		20.1	3.2
	27.5	3.5		24.3	3.5
	25.0	3.9		22.7	2.9
	22.5	3.1		23.9	3.8

Table 1: Roughness values after wire bristle impacting and after shot peening.

It can be seen that the roughness values are comparable. Wire bristle impacting gives rise to a maximum hardness value of slightly more than 180 HV0 1 (Fig. 5).

The penetration depth of increased hardness amounts to about 0.2 mm. As shown in figure 5, the micro-hardness distribution after shot peening is very similar.



Figure 5: Micro-hardness-depth profiles

As it is shown in figure 6, both surface treatments induce residual compressive stresses as measured by the hole drilling method. However, the magnitude of the residual compressive stresses after shot peening is markedly higher than after wire bristle impacting.



Figure 6: Residual stress profiles

The results of the rotating beam fatigue tests are depicted in figure 7. As opposed to the asturned reference condition, both surface treatments result in an enormous enhancement of the 10^7 cycles fatigue strength from about 125 MPa to more than 200 MPa (Fig. 7). Remarkedly, the fatigue strengths after shot peening and wire bristle impacting are very similar although the residual compressive stresses are rather different (Fig. 6).



Figure 7: S-N curves in rotating beam loading (R = -1)

Summary

Wire bristle impacting of precipitation hardened aluminum alloy Al2024-T4 leads to surface and surface layer properties surface roughness and microhardness-depth profiles very similar to conventional shot peening. The enhancement of the HCF strength due to wire bristle impacting can be as marked as due to shot peening although the shot peening induced residual compressive stresses are much higher.

References

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